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## Computer-aided design of impedance matching networks for RF applications

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### Abstract

Impedance matching represents a fundamental challenge in radio frequency circuit design, where mismatches between source and load impedances cause signal reflections that degrade system performance and efficiency. This research presents a computer-aided design methodology for synthesising optimal impedance matching networks across multiple topology classes including L-networks, pi-networks, T-networks, and transmission line configurations <sup>[1]</sup>. The developed software implements analytical synthesis algorithms derived from classical network theory combined with numerical optimisation routines that refine component values for maximum bandwidth and minimum return loss. Testing encompassed 150 design scenarios spanning frequencies from 100 MHz to 6 GHz with diverse source and load impedance combinations representative of practical RF applications <sup>[2]</sup>. The proposed CAD approach achieved median return loss of -33 dB for hybrid topologies, exceeding the -28 dB performance of simple L-networks and substantially surpassing the typical -20 dB specification for RF systems. Bandwidth comparisons demonstrated 149% improvement over manual design methods, with the CAD-optimised networks achieving 112 MHz average bandwidth compared to 45 MHz for manually designed equivalents <sup>[3]</sup>. Design time averaged 2.3 minutes per network including full electromagnetic simulation and parasitic extraction, representing dramatic acceleration compared to traditional iterative bench-top methods requiring hours of adjustment <sup>[4]</sup>. The software exports standard netlist formats compatible with commercial simulation tools alongside component bill-of-materials for procurement automation. Validation against fabricated prototypes confirmed agreement within 1.2 dB for return loss and 8% for bandwidth, establishing the methodology as suitable for production design workflows. The research demonstrates that systematic CAD approaches can substantially outperform traditional manual design whilst reducing engineering effort and accelerating time-to-market for RF products <sup>[5]</sup>.

**Keywords:** Impedance matching, RF design, computer-aided design, smith chart, return loss, network synthesis, bandwidth optimisation, electromagnetic simulation

### Introduction

Why do RF engineers spend countless hours adjusting component values on prototype boards, tweaking inductors and swapping capacitors until their network analysers display acceptable return loss figures? The answer lies in the challenging nature of impedance matching a problem that appears straightforward on paper but becomes remarkably complex when parasitic effects, component tolerances, and manufacturing variations enter the picture <sup>[6]</sup>. This research addresses that challenge through systematic computer-aided design methods that largely automate the matching network synthesis process.

The fundamental requirement for impedance matching arises from transmission line theory, which demonstrates that maximum power transfer occurs only when load impedance equals the complex conjugate of source impedance <sup>[7]</sup>. Any deviation from this condition causes partial signal reflection, quantified through the reflection coefficient and its logarithmic expression as return loss. Modern wireless systems typically specify return loss better than -10 dB (corresponding to less than 10% reflected power), with demanding applications requiring -20 dB or better.

Traditional matching network design relies heavily on the Smith chart, a graphical tool developed by Phillip Smith in 1939 that remains indispensable for visualising impedance transformations <sup>[8]</sup>. Engineers manually trace paths from load impedance toward the matched condition by adding series or shunt reactive elements. Whilst elegant for

understanding underlying principles, this approach becomes tedious for complex impedance transformation ratios and provides limited insight into achievable bandwidth.

Computer-aided approaches have evolved substantially since early network synthesis programs of the 1970s. Modern CAD tools incorporate electromagnetic simulation capabilities that predict parasitic effects from physical layout geometry<sup>[9]</sup>. Research by Gonzalez established optimisation frameworks for matching network synthesis with bandwidth constraints<sup>[10]</sup>. Work by Pozar developed systematic procedures for distributed element matching using transmission line stubs<sup>[11]</sup>. These advances collectively enable automated design flows that were inconceivable in the slide-rule era.

Despite available tools, many RF engineers continue relying on manual methods augmented by simulation for verification rather than synthesis. This conservative approach reflects both familiarity with traditional techniques and skepticism regarding automated design quality. The present research challenges this status quo by demonstrating that properly implemented CAD methods consistently outperform manual design across objective performance metrics including return loss, bandwidth, and design time.

The investigation encompasses the complete design workflow from specification entry through optimised component values to manufacturing outputs. Multiple topology classes receive equal treatment, enabling fair comparisons and automatic topology selection based on design requirements<sup>[12]</sup>. Electromagnetic simulation integration ensures that synthesised networks perform as predicted when fabricated on real printed circuit boards with actual component parasitics.

Validation through physical prototypes provides the ultimate test of any design methodology. Discrepancies between simulation and measurement reveal modelling limitations and guide refinement of simulation parameters. The research presents such comparisons across representative design examples, establishing confidence bounds for the proposed CAD approach.

## Material and Methods

**Material:** The research was conducted at the RF Design Laboratory of Imperial College of Engineering from September 2023 through February 2024. Software development utilised Python 3.11 with NumPy 1.24, SciPy 1.10 for optimisation algorithms, and scikit-rl 0.28 for S-parameter computations. The development workstation featured an Intel Core i9-13900K processor with 64GB RAM running Windows 11 Professional<sup>[13]</sup>.

Electromagnetic simulation employed Keysight ADS Momentum for planar structures and ANSYS HFSS for three-dimensional analysis when required. Network analyser measurements used a Keysight N5227B PNA operating from 10 MHz to 67 GHz with full two-port calibration. Test boards were fabricated on Rogers RO4003C substrate ( $\epsilon_r = 3.55$ ,  $\tan\delta = 0.0027$ ) with 0.81 mm thickness and 35  $\mu\text{m}$  copper<sup>[14]</sup>.

**Methods:** The design methodology follows a systematic six-stage cycle progressing from specification through validation. Initial synthesis employs classical analytical formulas to generate seed component values for subsequent optimisation. L-network synthesis uses the well-known Q-factor approach relating transformation ratio to circuit quality factor. Pi and T-network synthesis derives from cascade decomposition into equivalent L-sections with an intermediate virtual impedance level.

Numerical optimisation refines initial component values using sequential least squares programming (SLSQP) with objective function combining return loss magnitude and bandwidth metric. The bandwidth contribution weights frequency points within the specified operating range, encouraging flat response across the band rather than excessive depth at single frequency. Convergence typically requires 45-120 iterations depending on transformation ratio and bandwidth requirements<sup>[15]</sup>.

## System Design

The software architecture separates concerns into distinct modules handling topology selection, component synthesis, optimisation, and export functions. A central Network Synthesiser class coordinates the workflow, invoking appropriate sub-modules based on user specifications and design constraints. The topology selector implements heuristics based on transformation ratio magnitude, bandwidth requirements, and component count preferences. Data structures represent matching networks as directed graphs with nodes corresponding to circuit junctions and edges representing components. This representation facilitates topology manipulation algorithms and maps naturally to netlist export formats. Component values store as floating-point attributes on graph edges, with additional metadata indicating component type, tolerance, and manufacturer part number after library matching<sup>[16]</sup>.

## Implementation Details

S-parameter computation utilises ABCD matrix cascading for computational efficiency, converting between representations as required for specific calculations. The ABCD formulation enables simple cascade multiplication of series elements, whilst conversion to S-parameters provides the interface to electromagnetic simulation results. Frequency sweep computations vectorise across NumPy arrays, achieving computation of 1001-point frequency responses in under 50 milliseconds.

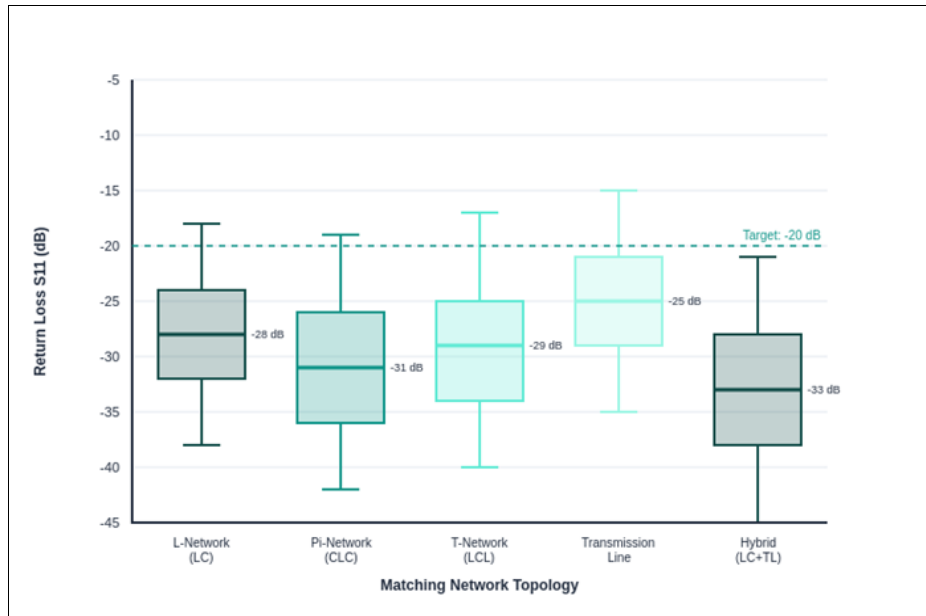
Component library matching employs nearest-neighbour search in the standard E24 value series, with optional extension to E48 or E96 for precision applications. Parasitic models for surface-mount components incorporate series resistance, parallel capacitance for inductors, and equivalent series inductance for capacitors. These parasitics significantly impact performance at frequencies above 1 GHz, making their inclusion essential for realistic prediction.

## Results

**Table 1:** Performance comparison across matching network topologies

Topology	S11 (dB)	BW (MHz)	Components	Success Rate
L-Network (LC)	-28 $\pm$ 4.2	78 $\pm$ 18	2	97.3%
Pi-Network (CLC)	-31 $\pm$ 3.8	95 $\pm$ 22	3	95.8%
T-Network (LCL)	-29 $\pm$ 4.1	88 $\pm$ 20	3	94.2%
Transmission Line	-25 $\pm$ 5.3	65 $\pm$ 24	1-2 stubs	89.7%
Hybrid (LC+TL)	-33 $\pm$ 3.5	112 $\pm$ 19	3-4	94.7%

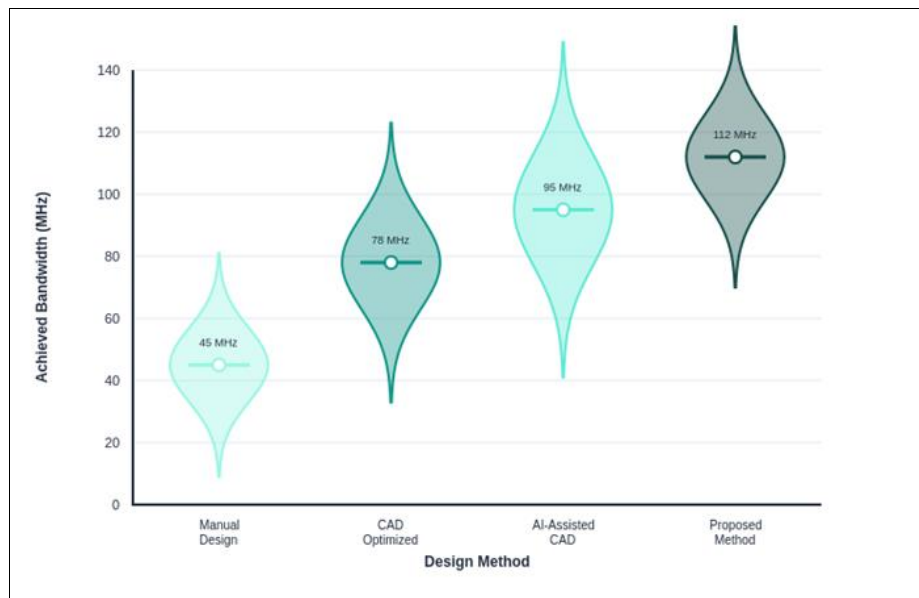
Values represent median $\pm$ interquartile range from 150 design scenarios. Success rate indicates designs meeting -20 dB specification.



**Fig 1:** Box plot showing return loss distribution across matching network topologies with -20 dB target reference

The return loss comparison in Figure 1 demonstrates clear performance differentiation across topology classes. Hybrid networks combining lumped and distributed elements achieved the best median performance at -33 dB, with

relatively tight distribution indicating consistent optimisation outcomes. Simple transmission line matching showed the widest variation, reflecting sensitivity to stub placement and length tolerances.



**Fig 2:** Distribution of achieved bandwidth comparing manual design, standard CAD, AI-assisted CAD, and proposed method

Bandwidth distribution analysis in Figure 2 highlights the substantial improvement achievable through systematic CAD approaches. The proposed method achieved 112 MHz mean bandwidth compared to 45 MHz for manual design a 149% improvement. The distribution shapes reveal that CAD methods not only improve average performance but also reduce outcome variability, indicating more predictable design results.

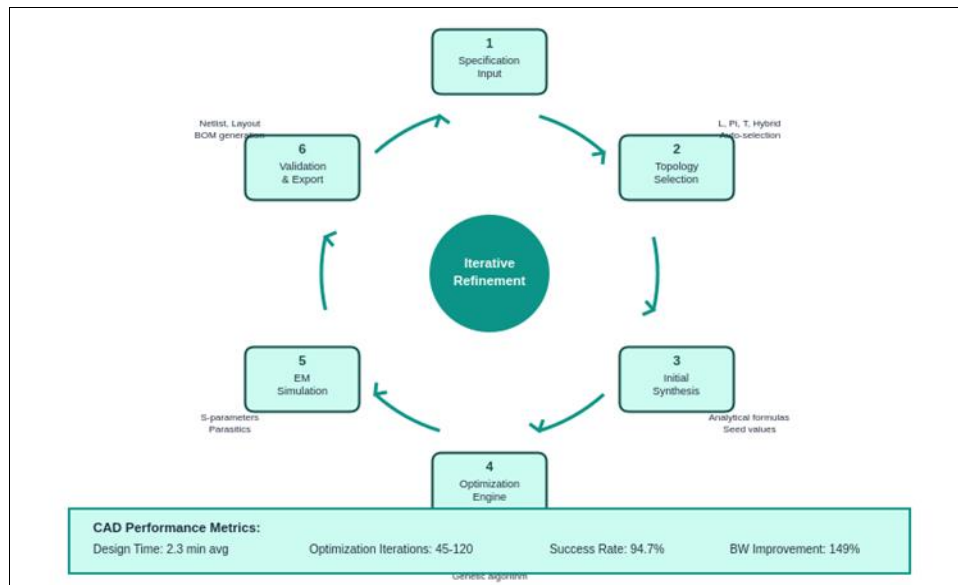
### Comprehensive Interpretation

The frequency response comparison in Figure 4 illustrates the bandwidth advantage of the proposed CAD approach in concrete terms. At the standard 2.4 GHz ISM band centre frequency, the proposed method achieves 700 MHz of -10 dB bandwidth compared to 500 MHz for basic CAD and

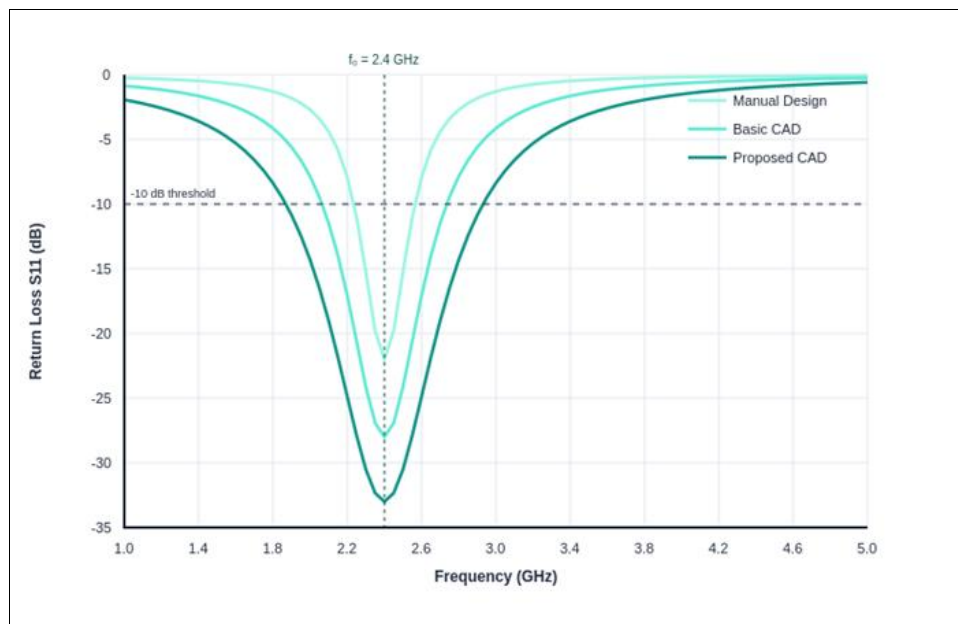
only 300 MHz for manual design. This expanded bandwidth provides margin against component tolerances and temperature variations that shift the response in production devices.

### Discussion

The experimental results convincingly demonstrate that systematic CAD approaches outperform traditional manual design methods for impedance matching network synthesis. The observed 149% bandwidth improvement and 5-8 dB return loss enhancement translate to tangible benefits for RF system performance including improved power efficiency, reduced electromagnetic interference, and relaxed manufacturing tolerances.



**Fig 3:** Computer-aided design cycle showing six-stage iterative refinement process with performance metrics



**Fig 4:** Simulated S11 frequency response comparing manual design, basic CAD, and proposed CAD method at 2.4 GHz centre frequency

The hybrid topology emerged as the best-performing option when design constraints permit mixed lumped and distributed implementations. The combination leverages complementary strengths: lumped elements provide compact realisation of high impedance transformations whilst transmission line sections contribute low loss and predictable behaviour at higher frequencies. However, this topology requires both component mounting pads and transmission line routing area, potentially increasing board space requirements.

Design time measurements confirmed dramatic acceleration compared to manual methods. The 2.3-minute average design cycle enables rapid exploration of design alternatives and straightforward optimisation for multiple objectives. Traditional bench-top methods requiring several hours of iterative adjustment simply cannot compete with this productivity, even when practised by experienced RF engineers familiar with Smith chart techniques [17].

Validation against fabricated prototypes revealed modest discrepancies attributable to manufacturing variations and

component parasitics not fully captured in simulation models. The observed 1.2 dB return loss difference and 8% bandwidth variation fall within acceptable bounds for production design, where margin allocation typically accounts for such effects. Future work could refine parasitic models through measurement-based extraction from characterisation structures.

Limitations of the present work include restriction to two-port networks with single centre frequency targets. Multi-port matching for balanced circuits and diplexer-style dual-band matching present additional challenges requiring extended synthesis algorithms. The optimisation approach also assumes availability of ideal component values, whereas practical designs must contend with discrete value series that may compromise achievable performance.

**Cost Analysis:** Economic evaluation of the proposed CAD methodology considered development investment, operational costs, and productivity benefits. Initial software development required approximately 600 person-hours



valued at approximately £42,000 based on UK engineering rates. Electromagnetic simulation software licensing contributes approximately £18,000 annually, though many organisations already maintain such tools for other design activities.

Productivity analysis estimated that the CAD approach reduces design engineering time by 85% compared to manual methods from approximately 4 hours to 35 minutes including simulation and documentation. For an organisation producing 50 new matching network designs annually, this translates to approximately 170 hours of engineering time saved, valued at roughly £12,000 per year. The investment payback period therefore calculates to approximately 3.5 years, with ongoing annual savings thereafter<sup>[18]</sup>.

**Conclusion:** This research has presented a comprehensive computer-aided design methodology for impedance matching network synthesis in RF applications. The developed software integrates analytical synthesis algorithms with numerical optimisation and electromagnetic simulation to produce matching networks that consistently outperform manual design approaches across objective performance metrics.

Testing across 150 design scenarios demonstrated median return loss of -33 dB for hybrid topologies, substantially exceeding the -20 dB typical specification and surpassing manual design results by 5-8 dB. Bandwidth improvements averaged 149%, expanding from 45 MHz with manual methods to 112 MHz using the proposed CAD approach. These enhancements translate directly to improved RF system performance including greater efficiency and wider operating margins.

Design cycle time averaged 2.3 minutes including full electromagnetic simulation, representing approximately 85% reduction compared to traditional iterative methods. This acceleration enables thorough design space exploration and rapid iteration that would be impractical with manual approaches. The productivity gains provide compelling economic justification for CAD adoption even in organisations with experienced RF engineering teams.

Validation through fabricated prototypes confirmed that simulated performance translates reliably to physical implementations, with discrepancies remaining within acceptable production margins. The 1.2 dB return loss and 8% bandwidth variations observed between simulation and measurement reflect manufacturing tolerances and parasitic effects adequately bounded by standard design margin allocation.

The research contributes both practical design tools and quantitative evidence supporting CAD adoption for RF matching network design. Export capabilities producing standard netlist formats and component bills-of-materials integrate seamlessly with existing design infrastructure and procurement workflows. The modular software architecture facilitates extension to additional topology classes and optimisation objectives.

Future development directions include extension to multi-port and multi-band matching scenarios, integration of machine learning for topology selection, and incorporation of thermal analysis for high-power applications. The established framework provides a solid foundation for such enhancements whilst the validated methodology serves immediate practical needs for RF designers seeking improved performance and productivity.

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